

Dependency of Evaporation and Class A Pan Coefficient on Meteorological Parameters



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Abstract

The relation of evaporation deriving meteorological parameters particularly wind speed, solar radiation and vapor pressure deficit with evaporation schemes namely Class A pan evaporation (E_p), potential evapotranspiration (PET) and reference evapotranspiration (ET_o) at Tharandt, Germany for the summer half-year of 2004-2013 was investigated. PET was calculated using three methods: 1. Haude (2005), 2. Wendling (1991), 3. Penman (1963); whereas, ET_o was calculated according to Food and Agricultural Organization-Penman Monteith method. The results showed that the evaporation schemes were mainly driven by solar radiation ($R^2 \geq 0.69$, $RMSE \leq 0.76 \text{ mm d}^{-1}$) and vapor pressure deficit ($R^2 \geq 0.53$, $RMSE \leq 0.92 \text{ mm d}^{-1}$). The effect of wind speed at 2m in deriving the evaporation schemes was negligibly small ($R^2 < 0.12$). An equation is derived for estimation of E_p from measured meteorological parameters alone which makes this study special. In another scenario, Class A pan coefficient (K_p) which is the ratio of ET_o and E_p had shown good correlation with E_p only ($R^2 = 0.50$, $RMSE = 0.19$, $n = 1483$). The correlation of K_p with ET_o , shortwave radiation, wind speed at 2m, vapor pressure deficit, relative air humidity, and air temperature was too low ($R^2 < 0.1$).

Keywords: Class A pan evaporation; Class A pan coefficient; Solar radiation; Vapor pressure deficit; Air temperature; Relative air humidity; Wind speed; Reference evapotranspiration; Potential evapotranspiration; Summer half-year; Tharandt

Abbreviations: E_p : Class A Pan evaporation; K_p : Class A Pan Coefficient; PET: potential evapotranspiration; ET_o : reference evapotranspiration; SHY: summer half-year which is the time from april to september; PETs: PET estimated according to Haude, Wendling, and Penman; R_n : net solar radiation; R_s : solar or shortwave or incoming radiation; u_2 : wind speed at 2m; VPD: vapor pressure deficit; RH: relative air humidity; T: air temperature; Haude7: PET calculated according to Haude in which 17 values which were greater than 7 mm d^{-1} are replaced by 7 mm d^{-1}

Introduction

Evaporation does not take place at a constant rate as its rate naturally depends on meteorological, geographical, and topographical factors. The principal meteorological parameters affecting evapotranspiration are solar radiation, air temperature, relative air humidity and wind speed (Trajković and Živković (2009) as cited in Isikwue BC et al. [1] p.698; also refer Moderow et al. [2] and Wang & Dickinson [3]. Vapor pressure deficit (i.e., air humidity and air temperature) is also one of the meteorological parameters which affect evaporation or evapotranspiration [4]. The rate at which molecules leave water depends on the vapor pressure of the water (e_w) and the rate at which molecules enter the air depends on the vapor pressure of the air (e_a) above the water surface. Thus, the rate of evaporation depends on the difference between them called vapor pressure deficit (VPD); i.e., $VPD = e_w - e_a$. Therefore, evaporation is proportional to $(e_w - e_a)$ and continuous until $e_w = e_a$. Similarly, evaporation is proportional to the difference between actual humidity and the saturated humidity at a given temperature.

In this article, the dependency of the methods of estimation of PET estimated according to Haude (Haude7), Wendling and Penman and ET_o estimated according to FAO56-PM method on wind speed at 2m (u_2), VPD, and shortwave and net solar radiation (R_s & R_n) at Tharandt from 2004 to 2013 for the summer half-year ($n = 1830$) was investigated. The summer half-year dependency of Class A pan evaporation (E_p) with u_2 , VPD, and R_s & R_n as well as with air temperature and with relative air humidity was also investigated ($n = 1709$).

Data and Methodology

The study area was Tharandt, Germany (altitude: 220 m a.s.l, latitude: $50^{\circ}58'42.06''$ N, longitude: $13^{\circ}34'52.69''$ E). Ten years (01.01.2004 to 31.12.2013) daily and ten minutes data of Tharandt meteorological station was the basis of the data set. The meteorological parameters and measurement devices used for the study are presented in Table 1.

Table 1: Primary and Secondary Meteorological data used for the study

Parameter	Notation	Measurement Device
relative humidity in % at 2 p.m.	$RH_{2pm,P}$	Psychrometer
air temperature in °C at 2 p.m.	T_{2pm}	Humidity Moisture Probe HMP45
relative humidity in % at 2 p.m.	RH_{2pm}	HMP45
air temperature in °C at 2 p.m.	$T_{2pm,rt}$	resistance thermometer (Pt100)
wind speed in $m\ s^{-1}$ at 3m above ground	u_3	Young Anemometer
Wind speed in $m\ s^{-1}$ at 10m above ground	u_{10}	Young Anemometer
Precipitation per day in mm (measured at 7 a.m.)	P	Hellmann mit Windring (verzinkt/V2A)
Precipitation per day in mm (automatic measurement at midnight): recorded every 10 minutes. A value of 144 indicates that for every interval of 10 min length a proper value was obtained. Values less than 144 indicate that the measurement device did not function in every time interval	RF	Precipitation gauge (Pluvio)
Global radiation measured at the roof of the Stöckhardtbau in $W\ m^{-2}$	$R_{s,roof}$	Pyranometer (CM7)
Global radiation in $W\ m^{-2}$ at 3m above ground	R_s	Pyranometer (SP Lite)
10 minutes values Water table height in mm	V'	Class-A pan (derived from pressure changes)
Maximum air temperature in °C	T_{max}	Thermometer
Minimum air temperature in °C	T_{min}	Thermometer
Maximum relative air humidity in % at 2m above ground	RH_{max}	HMP45
Minimum relative air humidity in % at 2m above ground	RH_{min}	HMP45
Daily values (7 a.m. to 7 a.m. of the next day) Water level height in mm	V	Class-A pan (derived from pressure changes)

(Source: Dr. Uta Moderow; TU Dresden, IHM, Chair of Meteorology).

The pan used for measurement of pan evaporation is the World Meteorological Organization (WMO) standard Class A pan evaporimeter (see Figure 1). Class A pan evaporation (E_p) is calculated as described in Mekoya et al. [6]. PET estimated using three methods:

a) Haude (2005) as cited in Weiß [7];

b) Wendling (1991) as cited in Wendling [8]; and

c) Penman (1963) as cited in ASCE-EWRI [9].

ET_o is estimated according to Allen et al. [10] (FAO56-PM). Net radiation (R_n) (in $MJ\ m^{-2}\ d^{-1}$) is also calculated as described in Allen et al. [10].

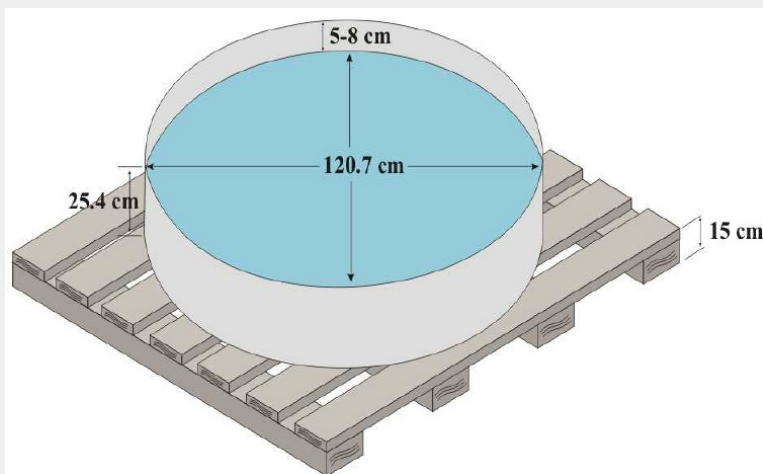


Figure 1: Appearance of Class A pan and its dimensions (source: Ertek [5], p.6708).

For the analyses, measured shortwave radiation in MJ m⁻² d⁻¹ at 3m above ground (R_s) was used. At Tharandt over the ten years (2004 to 2013) the average, extreme maximum and extreme minimum values of net radiation (R_n) were 8.87, 26.83 and 0.10MJ m⁻² d⁻¹; whereas its corresponding values of R_s were 6.19, 15.87 and -0.96MJ m⁻² d⁻¹, respectively.

Saturation vapor pressure (e_s) in kPa is calculated as given below.

$$e_s(T) = 0.6108 \cdot \exp\left[\frac{17.27}{(T + 237.3)}\right]; \quad [1] \quad (1)$$

Where, T is air temperature (in °C).

To get saturation vapor pressure (e_s) in hPa using T_{2pm}, Eq. 1 is modified as

$$e_s(T_{2pm}) = 0.6108 \cdot \exp\left[\frac{17.27 \cdot T_{2pm}}{(T_{2pm} + 237.3)}\right] \quad (1a)$$

Relative humidity in % (RH) expresses the degree of saturation of the air as a ratio of the actual (e_a) to the saturation (e_s) vapor pressure at the same temperature.

$$RH = 100 \cdot \frac{e_a}{e_s}; \quad [1] \quad (2)$$

Modifying Eq. 2 and replacing RH with RH_{2pm}, we have:

$$e_a = 100 \cdot \frac{RH_{2pm}}{e_s} \quad (3)$$

Generally, daily vapor pressure deficit (VPD) in kPa was calculated using Eq. 1 and Eq. 2. However, in the case of PET according to Haude, VPD in hPa was calculated using Eq. 1a and Eq. 3. Daily wind speed at 2 m above ground (u₂) in m s⁻¹ is calculated as given below.

$$u_2 = u_z \cdot \frac{4.87}{\ln(67.8z - 5.42)}; \quad [1] \quad (4)$$

$$u_z = \frac{u_z * 4.2}{(3.5 + \ln(z))}; \quad [8] \quad (5)$$

Where u_z is measured wind speed at z m above the ground surface (in m s⁻¹), and z is height of measurement above the ground surface (in m).

Daily wind speed at 2m above ground (u₂) in m s⁻¹ is used as calculated in Eq. 4 (except for PET according to Wendling which uses Eq. 5).

Finally, the degree of dependency of evaporation schemes on u₂, VPD, R_s and R_n was evaluated using a linear regression model where values of Pearson's correlation coefficient (r), R², RMSE, and p-value (at 95% confidence interval or at 0.05 significant level) were used for assessing the fit of the regression model.

Results and Discussions

Evaporation schemes and meteorological parameters

The dependency of evaporation schemes on wind speed

Figure 2 shows the dependency of potential evaporation schemes namely PET according to Haude, Haude7, Wendling and Penman with wind speed at 2m. Similarly, Figure 3 shows the dependency of reference evapotranspiration and Class A pan evaporation with u₂. Generally PET schemes, ET_o, and E_p had shown significantly poor dependency with u₂. The dependency was non-significant (p-value > 0.05) only in the case of PET estimated according to Haude7. Moreover, PETs, ET_o and E_p increased with increasing wind speed at 2m for u₂ ≤ 1 m s⁻¹ and slightly decreased with increasing values of u₂ for u₂ > 1 m s⁻¹, where in all cases R² was less than 0.1 (not shown).

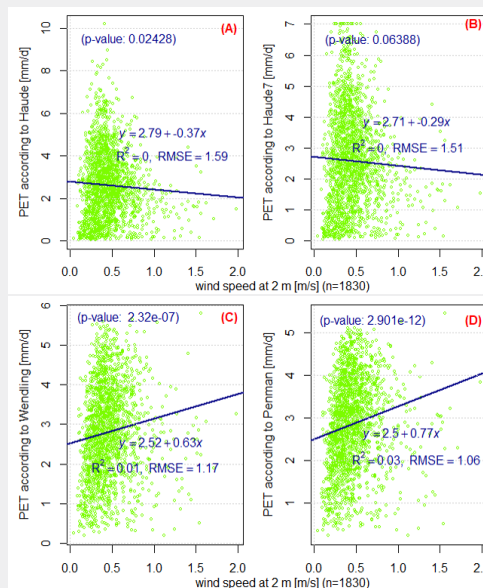


Figure 2: Dependency of PET estimated according to Haude (figure 'A'), 'Haude7' (figure 'B'), Wendling (figure 'C'), and Penman (figure 'D') on wind speed at 2m.

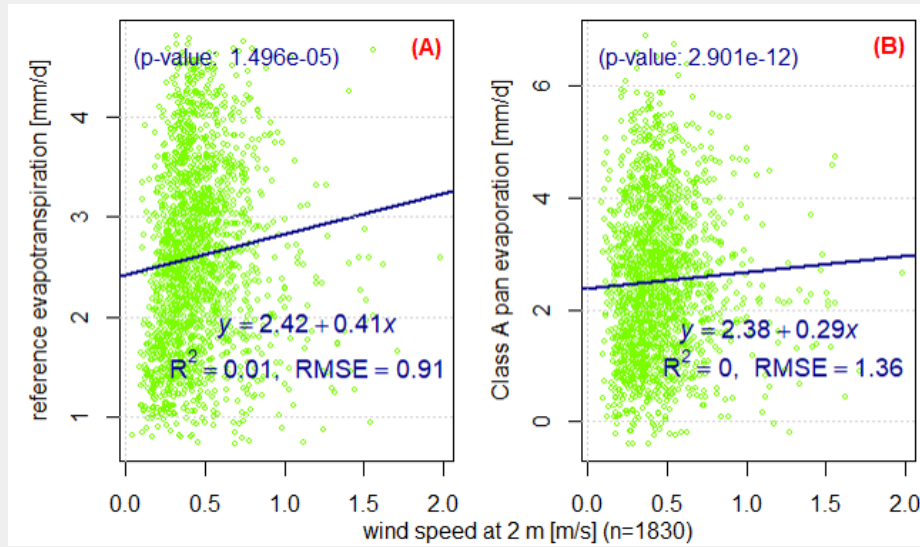


Figure 3: Dependency of reference evapotranspiration (figure 'A') and Class A pan evaporation (figure 'B') on wind speed at 2m

The dependency of evaporation schemes on vapor pressure deficit

The dependency of PETs and ET_0 with vapor pressure deficit was high ($R^2 \geq 0.78$; $RMSE \leq 0.62 \text{ mm d}^{-1}$) and significant ($p\text{-value} < 2.2 \cdot 10^{-16} < 0.05$); the dependency in the case of E_p was also 'slightly

strong' ($R^2 = 0.53$; $RMSE = 0.93 \text{ mm d}^{-1}$) and significant (see Figure 4 & 5). Particularly in the case of PET according to Haude it was extremely high ($R^2 = 0.98$; $RMSE = 0.23 \text{ mm d}^{-1}$) and significant. Note that PET according to Haude is calculated by multiplying calibrated factor and VPD.

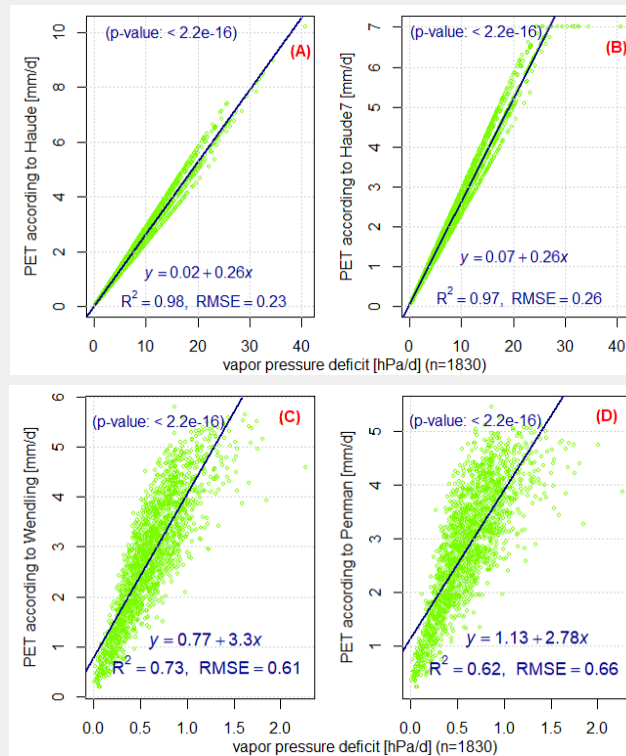


Figure 4: Dependency of PET estimated according to Haude (figure 'A'), 'Haude7' (figure 'B'), Wendling (figure 'C'), and Penman (figure 'D') on vapor pressure deficit.

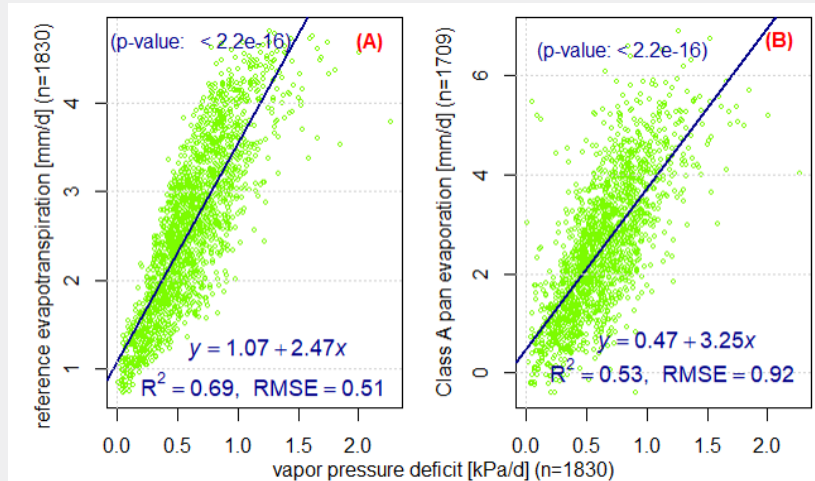


Figure 5: Dependency of reference evapotranspiration (figure 'A') and Class A pan evaporation (figure 'B') on vapor pressure deficit.

The dependency of evaporation schemes on solar radiation

Figure 6 & 7 show that the dependency of PETs and ET_0 on shortwave or solar radiation was high ($R^2 \geq 0.89$). The dependency of E_p on R_s was also a bit high ($R^2 = 0.69$; $RMSE = 0.76\text{mm d}^{-1}$).

The dependency was extremely high in the case of Penman and Wending PETs ($R^2 \geq 0.98$). The dependency of evaporation schemes on net solar radiation was very high and significant particularly in the case of ET_0 and PET according to Wending and Penman (see Table 2).

Table 2: Dependency of evaporation schemes on net solar radiation.

$y = ax+b$	ET_0	Penman PET	Wending PET	Haude PET
R^2	0.94	0.91	0.92	0.55
RMSE	0.23	0.32	0.33	1.07
a	0.31	0.4	0.41	0.42
b	-0.38	-0.97	-1.39	-1.35

Further on evaporation schemes and meteorological parameters

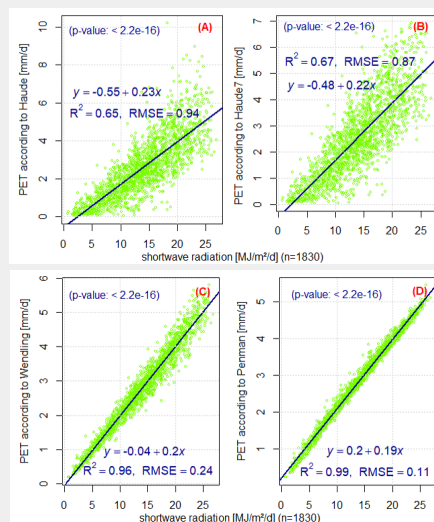


Figure 6: Dependency of PET estimated according to Haude (figure 'A'), 'Haude7' (figure 'B'), Wending (figure 'C'), and Penman (figure 'D') on shortwave radiation

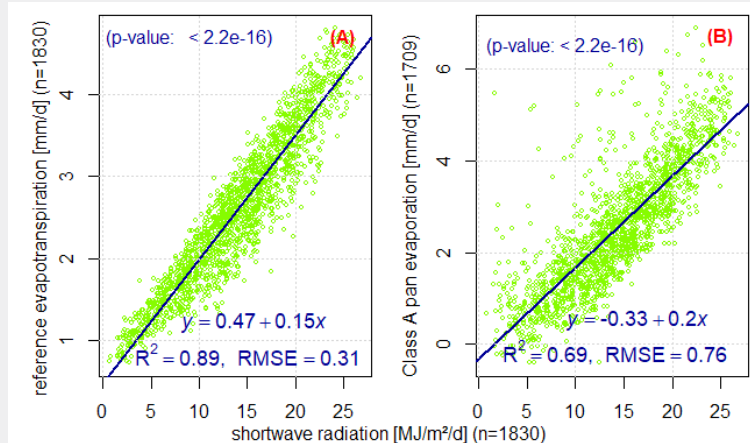


Figure 7: Dependency of reference evapotranspiration (figure 'A') and Class A pan evaporation (figure 'B') on shortwave radiation.

The relation between the evaporation schemes with maximum air temperature are presented in Figure 8 & 9. Generally, the correlation of the evaporation schemes with air temperature (not shown) was lower as compared to their correlation with maximum air temperature. A significant positive correlation ($r \geq 0.6$) was observed between all evaporation schemes and maximum air temperature. Also, the relation of air humidity with the

evaporation schemes is presented in Table 3, the corresponding graph for ET_0 and E_p is presented in Figure 10. For minimum relative air humidity and relative air humidity a significant good negative correlation ($r \leq -0.7$) was observed with all evaporation schemes except E_p (see Table 3 & 4). The intercorrelation between ET_0 , PET according to Wendling, and PET according to Penman was very high ($r > 0.9$).

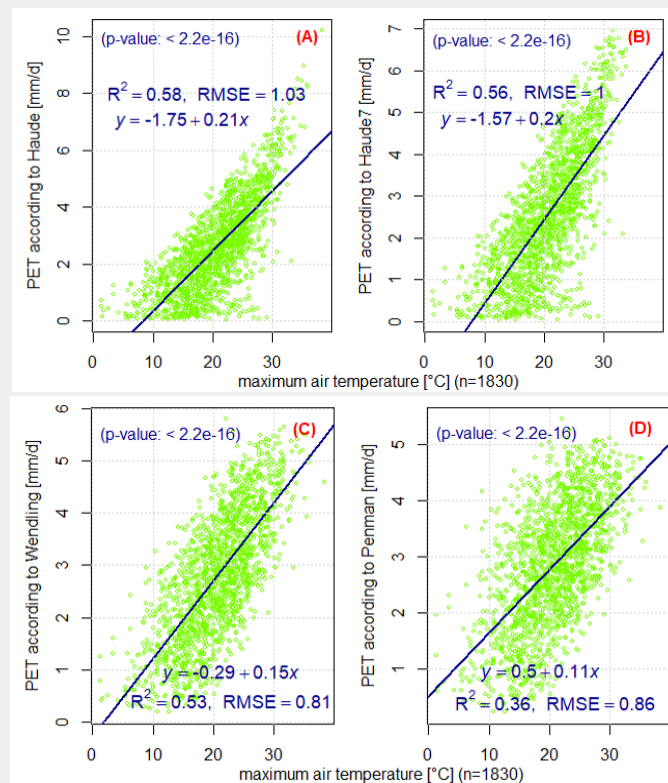


Figure 8: Relation between PET estimated according to Haude (figure 'A'), 'Haude7' (figure 'B'), Wendling (figure 'C'), and Penman (figure 'D') with maximum air temperature.

Table 3: Correlation between evaporation schemes with air humidity and with each other.

Correlation (r)	ET _o	Penman PET	Wendling PET	Haude PET
RH _{max}	-0.21	-0.29	-0.25	-0.26
RH	-0.67	-0.82	-0.77	-0.79
RH _{min}	-0.69	-0.84	-0.79	-0.81
ET _o	1	0.93	0.98	0.82
Penman PET	0.93	1	0.98	0.82
Wendling PET	0.98	0.98	1	0.86
Haude PET	0.82	0.82	0.86	1

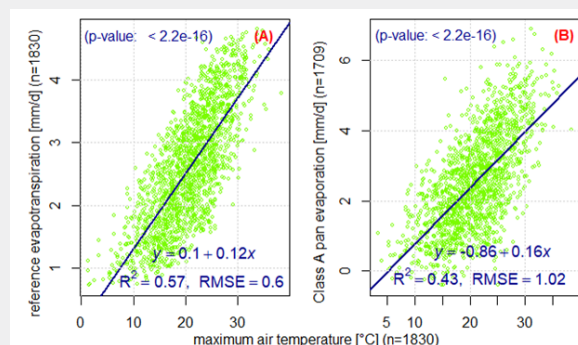


Figure 9: Relation between reference evapotranspiration (figure 'A') and Class A pan evaporation (figure 'B') with maximum air temperature

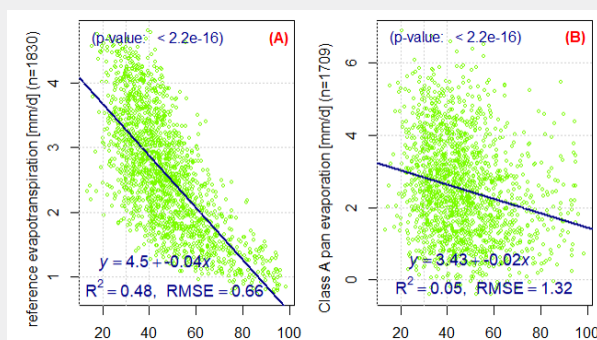


Figure 10: Relation between reference evapotranspiration (figure 'A') and Class A pan evaporation (figure 'B') with minimum relative air humidity.

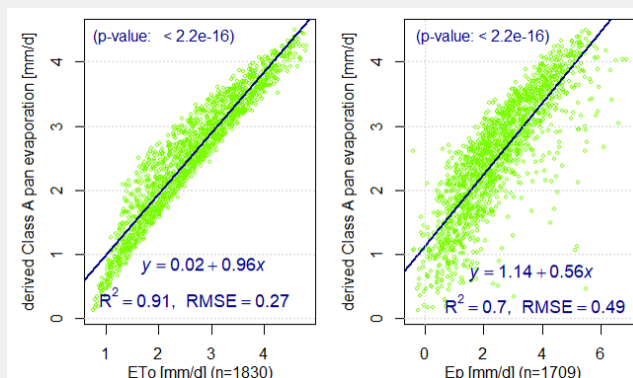


Figure 11: Relation between derived Class A pan evaporation with reference evapotranspiration and Class A pan evaporation.

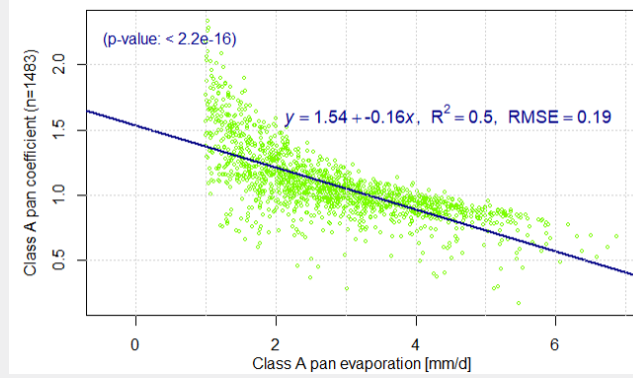


Figure 12: Dependency of Class A pan coefficient on Class A pan evaporation.

Table 4: Dependency of Class A pan evaporation on meteorological parameters.

y = ax+b	ET _o	R _n	R _s	K _p	VPD	T _{max}	RH _{min}	RH	T
r	0.88	0.84	0.83	0.71	0.73	0.66	0.6	0.59	0.58
R ²	0.78	0.71	0.69	0.5	0.53	0.43	0.36	0.35	0.34
RMSE	0.63	0.73	0.76	0.84	0.92	1.02	1.08	1.09	1.1
a	1.33	0.41	0.2	-3.09	3.25	0.16	-0.05	-0.09	0.18
b	-0.99	-1.39	-0.33	6.16	0.49	-0.86	5.01	9.16	-0.17
2(R ² +1- RMSE)	2.3	1.96	1.86	1.32	1.22	0.82	0.56	0.52	0.48

Derivation of equations for estimation of Class A pan evaporation

The Pearson’s correlation coefficient (r), R², RMSE, the slope (a), the y-intercept (b), and an accuracy factor ‘F’ = 2(R²+1- RMSE) of the linear regression model (‘y = ax + b’) described before are summarized in Table 4. F ranges from negative values to 4. Negative values of F indicate no accuracy and F = 4 indicates perfect alignment of model prediction or simulated or estimated data (y) and simulator or measured data (x). E_p can be estimated with good accuracy from ET_o, R_n, K_p, and VPD as given below, where y is replaced by E_p and x is replaced by ET_o, R_n, K_p, VPD, R_s, T_{max}, RH_{min}, RH and T.

$$E_{p_ET_o} = 1.33 ET_o - 0.99 \tag{6}$$

$$E_{p_R_n} = 0.41 R_n - 1.39 \tag{7}$$

$$E_{p_K_p} = 0.49 - 3.09 K_p \tag{8}$$

$$E_{p_VPD} = 3.25 VPD + 0.47 \tag{9}$$

However, the calculation of ET_o, R_n, K_p and VPD is not a simple task as it requires many parameters to be fulfilled. In contrast, estimation of E_p using only measured meteorological parameters such as R_s, T_{max}, RH_{min}, RH, and T which can be easily obtained from meteorological offices on request has been desired and are given below.

$$E_{p_R_s} = 0.2 R_s - 0.33 \tag{10}$$

$$E_{p_T_{max}} = 0.16 T_{max} - 0.86 \tag{11}$$

$$E_{p_RH_{min}} = 5.01 - 0.05 RH_{min} \tag{12}$$

$$E_{p_RH} = 9.16 - 0.09 R_s \tag{13}$$

$$E_{p_T} = 0.18 T - 0.17 \tag{14}$$

Comparatively relative air humidity (RH) and air temperature (T) have lower values of accuracy factor (F). Therefore, using weighted average of F and Eq. 10, Eq. 11 and Eq. 12, Class A pan evaporation (E_p) in mm d⁻¹ can be estimated with good accuracy from R_s, T_{max}, and RH_{min} as [1.86 (0.2 R_s - 0.33) + 0.82 (0.16 T_{max} - 0.86) + 0.56 (5.01 - 0.05 RH_{min})] / (1.86 + 0.82 + 0.56) ≈ (0.4 R_s + 0.13 T_{max} - 0.03 RH_{min} + 1.5) / 3.24 (see Eq. 15)

$$E_{pd} = (0.372 R_s + 0.1312 T_{max} - 0.028 RH_{min} + 1.4866) / 3.24 \tag{15}$$

Where, E_{pd} is Class A pan evaporations in mm d⁻¹ derived from measured solar or shortwave radiation (R_s) in MJ m⁻² d⁻¹, daily maximum air temperature (T_{max}) in °C, and daily minimum relative air humidity (RH_{min}) in %.

Class A pan coefficient and meteorological parameters

Class A pan coefficient (K_p) is the ratio of ET_o and E_p. Its correlation with meteorological variables such as solar radiations (R_s and R_n), vapor pressure deficit (VPD), wind speed at 2m (u₂), relative air humidity (RH) and air temperature (T) was too low (R² < 0.1). Also, the correlation between K_p and ET_o was too low (R² = 0.1; RMSE = 0.26). However, its correlation with E_p for E_p ≥ 1 mm d⁻¹ was relatively ‘good’ (R² = 0.50; RMSE = 0.19; n = 1483; see Figure 12).

On the basis of the result of the linear regression model, for Tharandt site and places with similar climatic and or topographic characteristic with Tharandt, a rough estimate of summer half-year daily values of K_p can be estimated from measured E_p (for 1 ≤ E_p ≤ 7.2 mm d⁻¹); range = [0.388, 1.38] (see Eq. 16).

$$K_p = 1.54 - 0.16 E_p \quad (16)$$

K_p can also be estimated from derived $E_p(E_{pd})$ (for $-0.5 \leq E_{pd} \leq 7.2 \text{ mm d}^{-1}$); range = [0, 1.54]

as $K_p = 1.44 - 0.2 E_{pd} \approx 1.44 - 0.2 (0.4 R_s + 0.13 T_{max} - 0.03 RH_{min} + 1.5) / 3.24$ (see Eq. 17 and Eq. 18).

$$K_p = 1.44 - 0.2 E_{pd} \quad (17)$$

$$K_p = 1.44 - 0.2 (0.372 R_s + 0.1312 T_{max} - 0.028 RH_{min} + 1.4866) / 3.24 \quad (18)$$

Where K_p is Class A pan coefficient and E_{pd} is derived Class A pan evaporation in mm d^{-1} .

Conclusion

At Tharandt for the summer half-year from 2004 to 2013 evaporation was mainly driven by solar radiation and vapor pressure deficit. The correlation between air temperature and relative air humidity with evaporation schemes was also good. Sunshine duration, which is not considered in this study, might also have good correlation with evaporation schemes. The effect of wind in deriving evaporation was negligibly too low. Moreover, the effect of wind speed at 2m (u_2) was not uniform. For $u_2 \leq 1 \text{ m s}^{-1}$, the evaporation schemes namely Class A pan evaporation, reference evaporation and potential evaporation (PET) according to Haude, Wendling and Penman increased with increasing values of u_2 , whereas, for $u_2 > 1 \text{ m s}^{-1}$, they slightly decreased with increasing values of u_2 . Note however that the cause for the negligibly too low effect of wind speed at 2m on evaporation schemes might have resulted due to topography of the study site. Because Tharandt station is located at the bottom of a 'V-shaped' valley in which there is a high shelter effect that could have an impact at least on the wind and sunshine duration. The non-uniform effect of wind speed (for $u_2 > 1 \text{ m s}^{-1}$ and for $u_2 \leq 1 \text{ m s}^{-1}$) on evaporation schemes is not clear. It might happen due to the influence of the nearby Weißeritz river.

The correlation between Class A pan coefficient and meteorological parameters such as solar radiation, vapor pressure deficit, wind speed at 2m, relative air humidity, air temperature and reference evapotranspiration was too low. However, its correlation with Class A pan evaporation (E_p) was comparatively good. Thus, for Tharandt site and places with similar climatic and topographic characteristics with Tharandt, Class A pan coefficient can be estimated from E_p alone with good accuracy. Also, at Tharandt, for the summer half-year E_p can be estimated from reference evapotranspiration, net solar radiation, Class A pan coefficient, vapor pressure deficit, solar or shortwave radiation, maximum air temperature, minimum relative air humidity, relative air humidity, and air temperature with very good accuracy. Particularly, the estimation of Class A pan evaporation merely based on measured solar radiation, maximum air temperature and minimum relative humidity makes this study special. Inclusion of actual sunshine duration hours which might improve the accuracy of the estimation of Class A pan evaporation is recommended.

The results of this study can be used for other parts of the world; however, only after proper validation because for

instance unlike the case in Tharandt, in other parts of the world, the contribution of wind speed in deriving evaporation (evapotranspiration) maybe even higher than vapor pressure deficit. Note also that the equations developed in this study are based on ten years of climate data of a single station. Therefore, the results of this article shall be evaluated again using at least thirty years of climate data from multiple stations, if available, as ten years may not be enough to draw a generalized and strong conclusion. Last but not least, the knowledge obtained from this study may be used for evaporation related study in Tharandt and in areas with similar climatic conditions with Tharandt which can serve for decision makers to take appropriate measures in various agriculture, water and forestry sectors. Because summer half-year evaporation and precipitation amounts were almost equal, this study can also be implemented in warmer areas of the world with some modifications.

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Data Availability Statement

All data used during the study were provided by a third party. Direct requests for these materials may be made to the provider as indicated in the Acknowledgements. Also, all models or code generated or used during the study are available from the corresponding author by request.

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