



Mini Review

Volume 3 Issue 1 - May 2018  
DOI: 10.19080/RAEJ.2018.03.555605

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# Angular Parameterization of Orthonormal Wavelet Filter Banks in Power Quality: A Method for Detecting Disturbances in the Voltage Waveforms



Diniz HC<sup>1</sup>, Uzinski JC<sup>2</sup> and Ferrari JGP<sup>2\*</sup>

<sup>1</sup>Department of Electrical Engineering, Universidade Estadual Paulista, Brazil

<sup>2</sup>Department of Electrical Engineering, Universidade do Estado de Mato Grosso, Brazil

Submission: February 07, 2018; Published: May 29, 2018

\*Corresponding author: Uzinski JC, Universidade do Estado de Mato Grosso, Rua das Gaivotas-325, Jardim das Nações-Sinop, Brazil, Tel: 5518 998030688; Email: uzinski.julio@unemat.com

## Abstract

Detecting transients in the voltage waveforms is one of the most important issues in power quality for both the preservation of equipment connected to the network, as well as the power supply. Among various techniques for detection of transients in electrical signals highlights, the wavelet transform is a method that can determine the instant when the disturbances occur and can detect different types in a same signal. The orthonormal wavelet filter banks yield a perfect reconstruction of a decomposed signal and if the regularity of the used wavelets is high, where the compression of the regular parts of the signal is good, and better evidencing of the singularities is at hand. In this paper, an orthonormal wavelet filter banks parameterization for detecting disturbances in the voltage waveforms is proposed. To evaluate the proposed methodology, some tests of detecting singularities in the voltage waveforms are presented.

**Keywords:** Angular parameterization; Orthonormal wavelet; Filter banks; Power quality; Waveforms; Voltage; Electrical signals.

## Introduction

The power quality is a major concern of energy suppliers, equipment manufacturers, and users in general. Problems in power quality can be defined as any phenomenon that occurs in voltage, current or frequency deviation, resulting in failure or improper operation of equipment connected to the network.

Transitional situations in power systems are common and may occur due to lightning strikes, fault current, starting currents of large motors, or due to capacitor switching [1].

Such disturbances that arise in the system can cause several unwanted interference as sensitive equipment malfunction, distortions in measurement equipment, and even they can result in the interruption of power supply. What results in losses both for the energy concessionaires as for the consumers. Due to the increased use of electronic devices, it becomes increasingly necessary the care to the energy quality provided by the power utility [2].

In this paper, a sinusoidal waveform representing the voltage with a duration of 5 seconds is used, Figure 1, which is a signal in its ideal form, this is, without disturbance or interference. From this signal, the signals with disorders which is used in this work have been generated

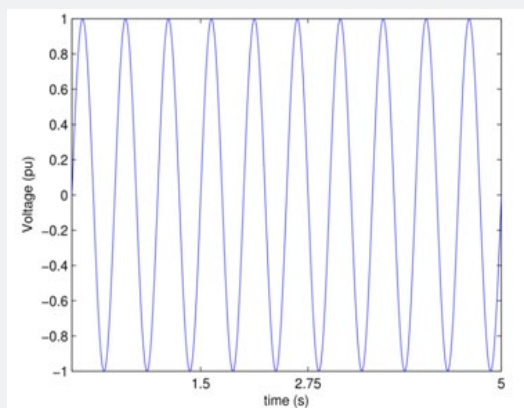


Figure 1: Signal in its ideal form (without disturbance).

## Short term voltage fluctuations

Variations are considered as a short term duration when the duration is between 0, 5 cycle to 1 minute, whereas, these voltage variations are generated by energization of large loads or intermittent failures in the connections of the system cables. The failures that may occur in these situations are a sag, a voltage elevation, or complete interruption of the electrical system [2]

**SAG:** The voltage sag, is characterized as the occurrence of a brief drop in the effective voltage value for a certain time interval. Depending on the location of the fault and system conditions, a fault may cause a temporary decrease of 10 to 90% in the effective value of the system voltage [3]. If the system voltage falls 30% or more, its condition is considered critical [4]. It is shown in Figure 2, a sag disturbance that lasts for three cycles.

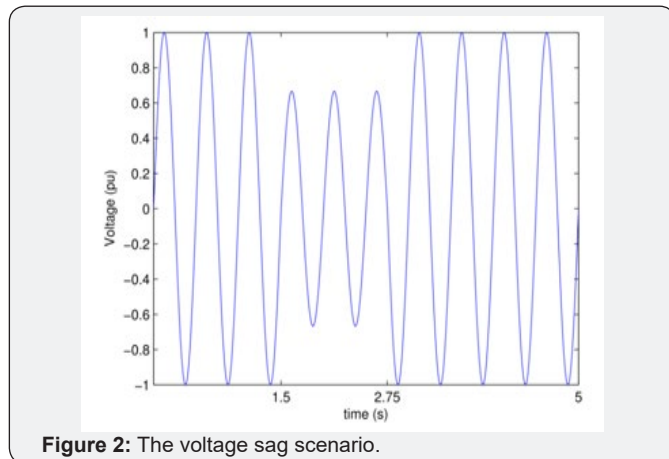


Figure 2: The voltage sag scenario.

This kind of disturbances usually occur by faults in transmission and distribution systems, and also it may arise due to energization of heavy loads, starting of large motors or the energizing of a transformer [2].

**Voltage Elevation (Swell):** Unlike the sag disturbance event, the voltage elevation (Swell) is characterized by a little increase in the system effective voltage, it is possible to occur an increase of 10% to 80% of the voltage, with duration of 0, 5cycle to 1 minute [3]. This shortfall may stress the delicate equipment components to premature failure.

This type of disorder can also be generated by system faults, and mainly with the phase-to-ground short-circuit. Also it may occur due to output of large blocks of loads or the energization of large capacitor banks, however, with a lower incidence [2]. The waveform of voltage swell is shown in Figure 3.

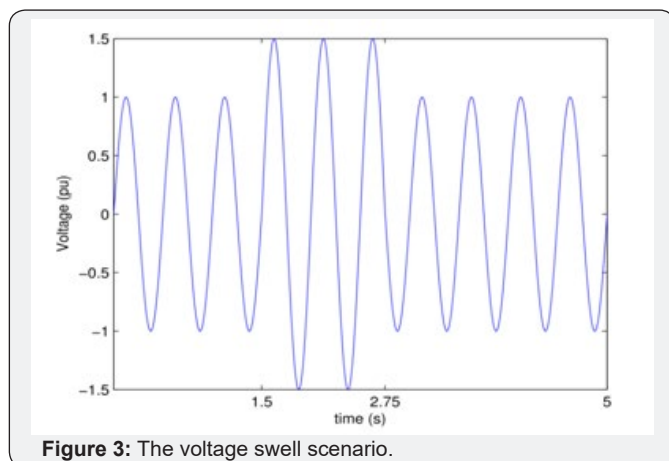


Figure 3: The voltage swell scenario.

**Interruption:** The interruption of short duration is characterized as a momentary loss of voltage on a power system. An interruption which reveals a drop of 90% to 100% of the system voltage lasting for half a cycle to 1 minute is caused by faults in the power system, equipment failures and malfunctions of control systems [2].

It is also possible that the interruption occurs immediately after a voltage sag, which usually happens due to faults in the supply system. Sag will occur between the fault inception and operation of the protective device system. Figure 4 shows an example of interruption applied to the presented signal of Figure 1 [2].

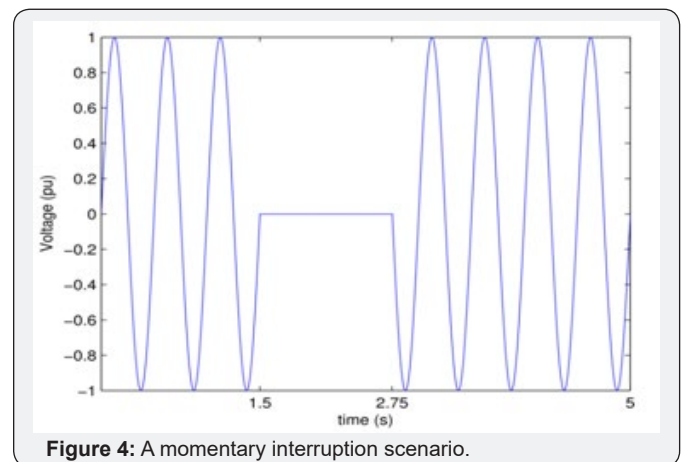


Figure 4: A momentary interruption scenario.

### Long term voltage fluctuations

Voltage variations are characterized as long-term when it occurs for a period of more than 1 minute. Having similar characteristics with the variations of short duration and usually caused by load variations and switching operations in the system.

### Wavelet Transform - WT

The Wavelet Transform (WT) is a tool that allows the unification of a large number of techniques for analysis and processing. The development of wavelet theory occurred in the fields of Mathematics, Engineering and Quantum Physics. Currently may be included in: seismic geology, image processing, computational and human vision, radar and sonar, spectrometry, computer graphics, analysis of transients in power lines, and other applications [5].

A wavelet is a function  $\psi(t) \in L^1(\mathbb{R}) \cap L^2(\mathbb{R})$ , such that the family of functions

$$\psi_{j,k}(t) = 2^{-j/2} \psi(2^{-j}t - k),$$

Where  $j$  and  $k$  are arbitrary integers as an orthonormal basis for  $L^2(\mathbb{R})$ . If  $\psi(t)$  is a wavelet, then  $\psi_{j,k}(t)$  is too for any  $j, k \in \mathbb{Z}$ .

The Wavelet Transform is written in the form:

$$(T^{WAV} f)(a, b) = |a|^{-\frac{1}{2}} \int f(t) \psi\left(\frac{t-b}{a}\right) dt \quad (1)$$

In (1) the values of  $a$  and  $b$  for the discrete values  $a = a_0^m$  and  $b = nb_0a_0^m$  are restricted, where,  $m, n \in \mathbb{Z}$  and  $a_0 > 1, b_0 > 0$  are constants has

$$T_{m,n}^{WAV}(f) = a_0^{-m/2} \int f(t) \psi(a_0^{-m}t - nb_0) dt \quad (2)$$

The parameter  $b$  indicates the translation of the length in  $b$  the axis  $t$ , it is concluded that (1) provides a time-frequency description for  $f$ . The parameter  $a$  is the scale parameter.

The function  $\psi_{a,b}(t)$  has time and width adapted to its frequency: the  $\psi_{a,b}(t)$  under high frequency conditions is 'narrower', while under low frequencies, they are broad. This makes that the wavelet transform be more efficient for local analysis of short duration phenomena with high frequency, that not characterize stationary signals, such as transient in signals [6].

### Formulation of sherlock & monro

The angular parameterization of orthonormal filter bank was initially studied in [7], adapting the work of [8] in factorization of paraunity matrix and parameterizing the orthonormal wavelet space by a set of angular parameters. This parameterization can be used to adjust the wavelet, in order to improve the performance index of certain applications related to signal processing concerned.

The weights of the low-pass filter  $H$  and high-pass filter of the filter bank are  $h_i^{(N)}$  and  $g_i^{(N)}$ , and the transfer functions of these filters are given respectively by

$$H^{(N)}(z) = \sum_{i=0}^{2N-1} h_i^{(N)} z^{-i} \quad (3)$$

$$G^{(N)}(z) = \sum_{i=0}^{2N-1} g_i^{(N)} z^{-i} \quad (4)$$

where the length of the filter bank is  $2N$ .

To ensure the condition of complementarity between  $H$  and  $G$ , so that the FWT is invertible, the weights of  $g_i^{(N)}$  are obtained from  $h_i^{(N)}$  through a method called of 'AlternateFlip' in [9] as follow,

$$g_i^{(N)} = (-1)^{i+1} h_{2N-1-i}^{(N)} \quad i = 0, 1, \dots, 2N-1 \quad (5)$$

It follows that the orthogonal filter pairs can be completely parameterized by  $N$  angles  $\alpha_i, 1 \leq i \leq N$ , that can take any value in the set of real numbers, [10].

In the formulation of [7] and using [8], a recursive formulas to express the coefficients of  $h_i^{(N)}$  are presented

$$\begin{aligned} h_0^{(1)} &= \cos(\alpha_1) \\ h_1^{(1)} &= \sin(\alpha_1) \\ h_0^{(N+1)} &= \cos(\alpha_{N+1}) h_0^{(N)} \\ h_{2i}^{(N+1)} &= \cos(\alpha_{N+1}) h_{2i}^{(N)} - \sin(\alpha_{N+1}) h_{2i-1}^{(N)} \end{aligned} \quad (6)$$

$$h_{2N}^{(N+1)} = -\sin(\alpha_{N+1}) h_{2N-1}^{(N)}$$

$$h_1^{(N+1)} = \sin(\alpha_{N+1}) h_0^{(N)}$$

$$h_{2i+1}^{(N+1)} = \sin(\alpha_{N+1}) h_{2i}^{(N)} + \cos(\alpha_{N+1}) h_{2i-1}^{(N)}$$

$$h_{2N+1}^{(N+1)} = \cos(\alpha_{N+1}) h_{2N}^{(N)}$$

where  $i = 0, 1, \dots, 2N-1$ .

According to [11-13], the parameterization based on (6) satisfies the conditions for orthonormality presented in [9],

$$\sum_{i=0}^{2N-1} [h_i^{(N)}]^2 = 1, N \geq 1, \quad (7)$$

$$\sum_{i=0}^{2N-1-2m} h_i^{(N)} n_{i+2m}^{(N)} = 0, m = 1, 2, \dots, N-1 \geq 2 \quad (8)$$

### Regularity of sherlock & monro wavelets

An important factor to be considered is the choice of the wavelet that should be used in the analysis of a given signal. In the decomposition of a signal by WT, properties such as regularity, smoothness and compact support are deterministic in the choice of wavelet to be used. The greater the number of vanishing moments of a wavelet, the smoother it is.

The formulation of [7] guarantees the orthonormality of the filter bank, on the other hand, it does not guarantee that the parameterized wavelet has a number of pre-determined vanishing moments; in this sense, [10] extend the formulation and present restrictions to guarantee up to two vanish moments and in [11-13] the authors has made the extension to vanishing moments of at least three.

According to [7], in order to characterizing the WT filter bank and considering at least one vanishing moment it is necessary to taking into account the (9).

$$\alpha_n = \frac{\pi}{4} - \sum_{i=1}^{N-1} \alpha_i \quad (9)$$

In order that the WT has at least two vanishing moments it is necessary to consider (10).

$$\alpha_{N-1} = \frac{1}{2} \arcsin \left\{ -\frac{1}{2} - \sum_{i=1}^{N-2} \left[ \sin \sum_{j=1}^k 2\alpha_j \right] \right\} - \sum_{i=1}^{N-2} \alpha_i \quad (10)$$

Equation (10) has a real solution if the angles  $\alpha_i$  satisfy the condition of (11).

$$-\frac{3}{2} \leq \sum_{i=0}^{N-2} \left[ \sin \sum_{j=1}^k 2\alpha_j \right] \leq \frac{1}{2} \quad (11)$$

According to [11-13], continuing with the reasoning, in order to obtain a third vanishing moment it is necessary to satisfy (12)

$$\alpha_{N-2} = \frac{1}{2} \arcsin \left\{ -\sum_{j=1}^{N-1} \left\{ \frac{1}{2} \sin \lambda_j + N \cos \lambda_j \right\} - \sum_{j=1}^{N-3} \left\{ \sum_{k=1}^{N-j-1} \sin \lambda_k \right\} - \frac{N}{2} \right\} - \sum_{i=2, i \neq N-2}^{N-1} \alpha_i \quad (12)$$

$$\text{where } \lambda_j = \left[ 2 \sum_{i=(N-j)+1}^N \alpha_i \right] e^{\lambda_k} = \left[ 2 \sum_{i=k+1}^{k+j} \alpha_i \right]$$

The equation (12) ensures the third vanishing moment, but the equation (12) has a real solution if the angles  $\alpha_i$  satisfy the condition of (13)

$$-1 \leq \left\{ \sum_{j=1}^{N-1} \left\{ \frac{1}{2} \sin \lambda_j + N \cos \lambda_j \right\} + \sum_{j=1}^{N-3} \left\{ \sum_{k=1}^{N-j-1} \sin \lambda_k \right\} + \frac{N}{2} \right\} \leq 1 \quad (13)$$

### Detection of the Aggregated Disorders in the Voltage Waveforms

According to this idea and the previous restrictions, especially (12), a wavelet was obtained with three null moments. This wavelet is given from the set of angular parameters  $\alpha = \{-0.3033, -0.8243, 1.6308, 0.2822\}$  and is denoted by  $\psi$ , which is shown in Figure 5.

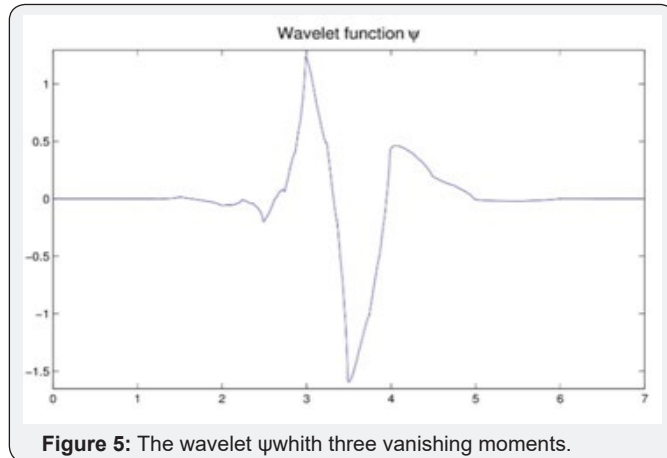


Figure 5: The wavelet  $\psi$  with three vanishing moments.

First, the signal presented without disturbances, Figure 1, was analyzed using  $\psi$ . The Figure 6 shows the detail coefficients of the analyzed signal in the first (d1) and second (d2) decomposition levels using  $\psi$ . In the Figure 7, the scalogram which represents the percentage of energy for each wavelet coefficient is considered [14].

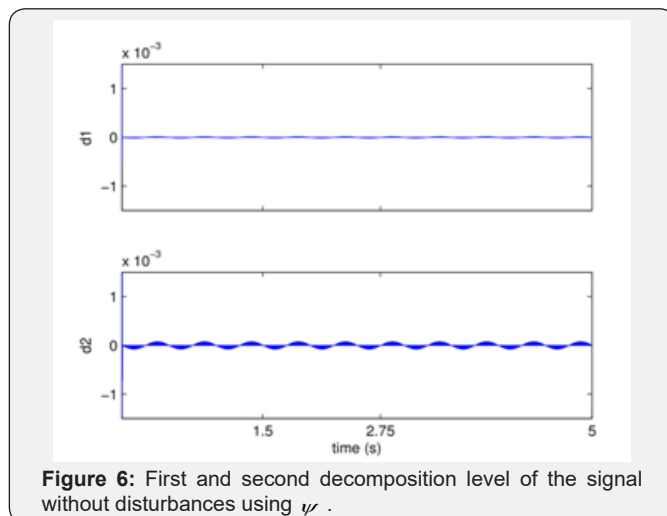


Figure 6: First and second decomposition level of the signal without disturbances using  $\psi$ .

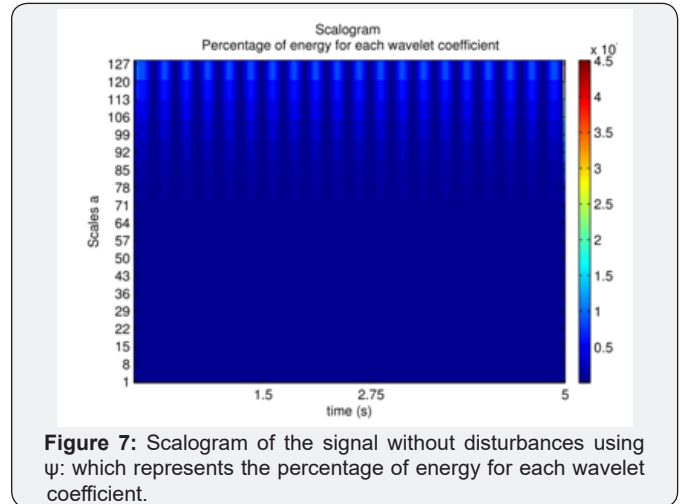


Figure 7: Scalogram of the signal without disturbances using  $\psi$ : which represents the percentage of energy for each wavelet coefficient.

In the Figure 6, it can be seen that there is no presence of the detail coefficients with higher amplitude suggesting the absence of high frequency information. The concept of Figure 7 is the same as Figure 6, because there is no evidence of energy change at different times. This is expected since the signal is decomposed into ideal conditions, that is, without disturbances.

After analyzing the signal without disturbances, the analysis of signals with SAG, swell and interruption are made. In these cases the presented singularities in the voltage waveforms should be located according to the time in which they occur.

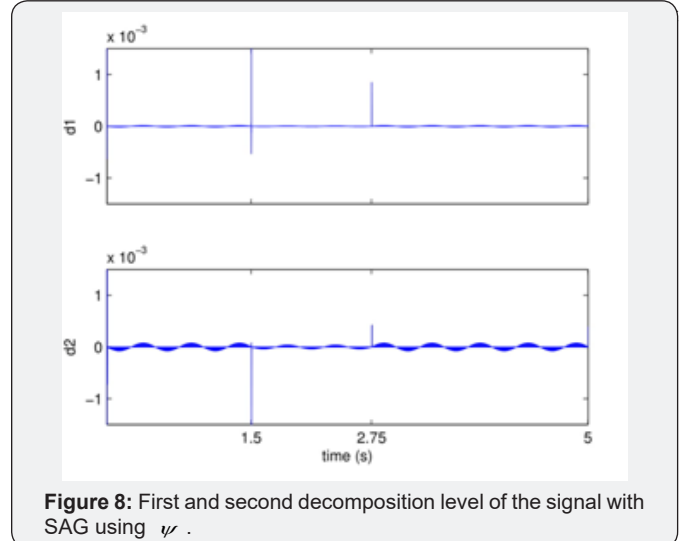
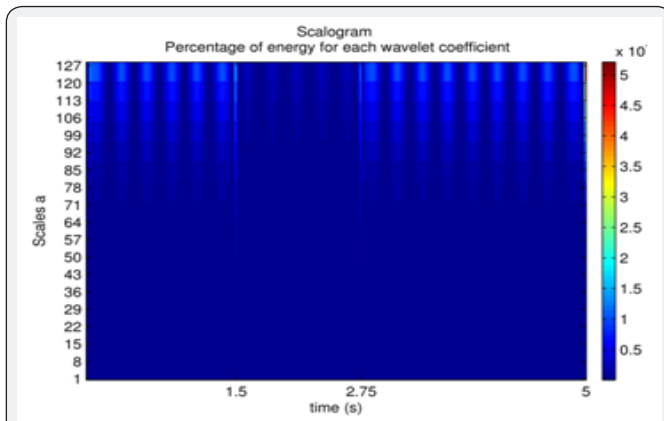
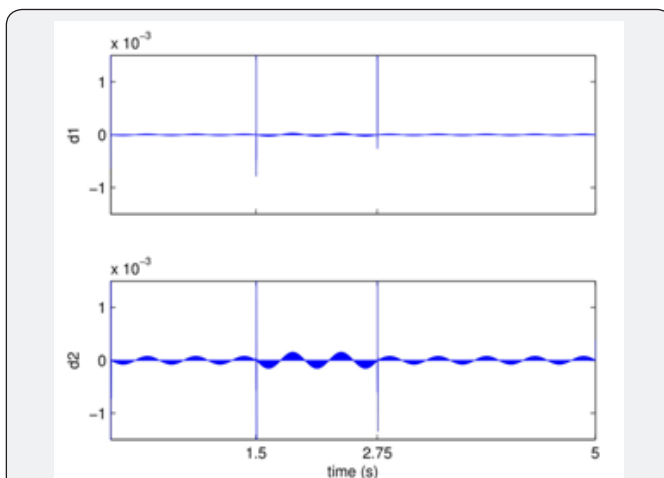


Figure 8: First and second decomposition level of the signal with SAG using  $\psi$ .

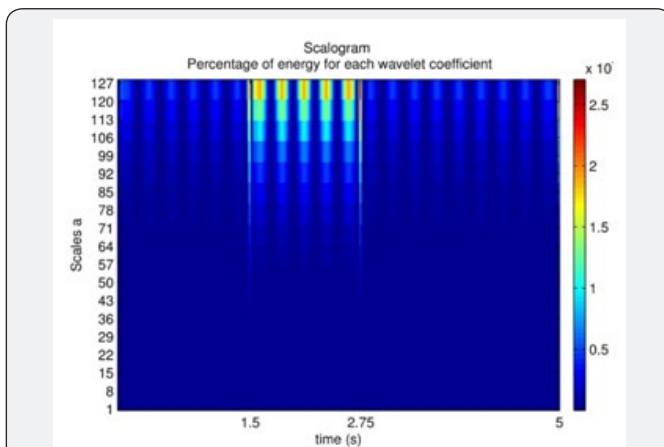
Figure 8 reveals the presence of detail coefficients with greater amplitude at instants 1.5s and 2.75s, interval in which the SAG phenomenon occurs. The other parts of the signal are more regular, but in the interval  $1.5s < t < 2.75s$  the amplitude of the detail coefficients is slightly smaller which in  $0s \leq t < 1.5s$  and  $2.75s < t \leq 5s$ . The Figure 9 is the best evidence of it, because it is observable that the percentage of energy in the range  $1.5s < t < 2.75s$  is lower than of  $0s \leq t < 1.5s$  and  $2.75s < t \leq 5s$ , indicating the presence of a dip in the signal. Therefore through both figures it is concluded that at 1.5s minute starts a SAG which ends in 2.75s.



**Figure 9:** Scalogram of the signal with SAG using  $\psi$ : which represents the percentage of energy for each wavelet coefficient.



**Figure 10:** First and second decomposition level of the signal with swell using  $\psi$ .

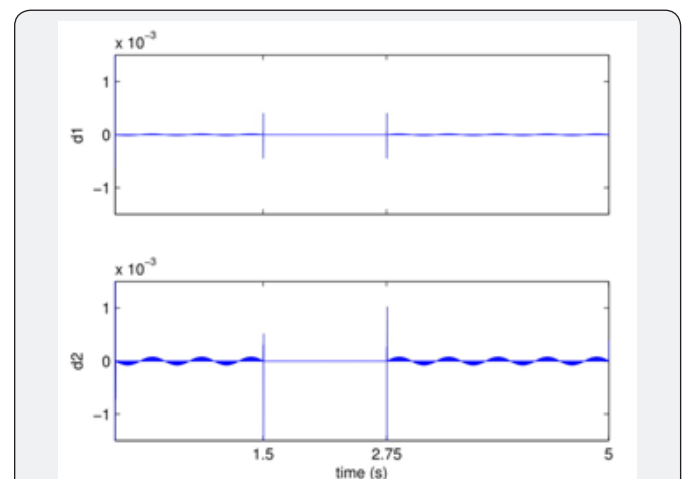


**Figure 11:** Scalogram of the signal with swell using  $\psi$ : which represents the percentage of energy for each wavelet coefficient.

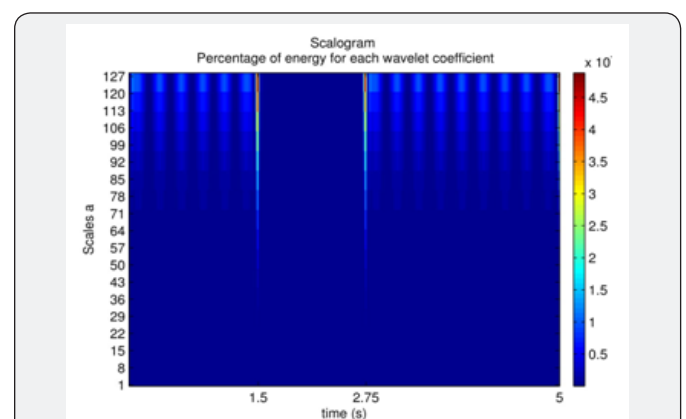
The signal with swell, Figure 3, was also analyzed using the wavelet  $\psi$ , Figure 5, with three vanishing moments. The decomposed signal in the first (d1) and second (d2) level is shown in the Figure 10. In the Figure 11 the scalogram is considered which represents the percentage of energy for each wavelet coefficient.

From Figure 10 the presence of detail coefficients with greater amplitude at instants 1.5s and 2.75s, interval in which the swell phenomenon occurs is realized. The other parts of the signal are more regular, but in the range  $1.5s < t < 2.75s$  the amplitude of the detail coefficients is slightly lower which  $0s \leq t < 1.5s$  and  $2.75s < t \leq 5s$ . From Figure 11 it is more understandable the meaning of it, because it is observable the percentage of energy in the range  $1.5s < t < 2.75s$  is higher than in  $0s \leq t < 1.5s$  and  $2.75s < t \leq 5s$ , indicating the presence of a swell in the signal. Therefore through both figures we conclude that the instant 1.5s minute starts a swell which ends in 2.75s.

The signal with an interruption, Figure 4, was analyzed using the wavelet  $\psi$ , Figure 5, with three vanishing moments. The decomposed signal in the first (d1) and second (d2) level is shown in the Figure 12. In the Figure 13 the scalogram is considered which represents the percentage of energy for each wavelet coefficient.



**Figure 12:** First and second decomposition level of the signal with interruption using  $\psi$ .



**Figure 13:** Scalogram of the signal with interruption using  $\psi$ : which represents the percentage of energy for each wavelet coefficient.

In the Figure 12 the presence of detail coefficients with greater amplitude at instants 1.5s and 2.75s, interval in which the interruption occurs is realized. The other parts of the signal



are more regular, but in the interval  $1.5s < t < 2.75s$  the amplitude of the detail coefficients is zero differently that in  $0s \leq t < 1.5s$  and  $2.75s < t \leq 5s$ . The Figure 13 shows better the meaning of it, because it is visible the percentage of energy in the interval  $1.5s < t < 2.75s$  is zero, as opposed that in  $0s \leq t < 1.5s$  and  $2.75s < t \leq 5s$ , indicating the presence of an interruption in the signal. Therefore, from Figures 12 & 13 we conclude that at the instant 1.5s starts an interrupt ending on 2.75s.

## Conclusion

In this paper, signals with disturbances in the voltage waveform presented in the study of power quality are analyzed. To ensure the operation of equipment connected to the network the detection of these disorders is important, so it is interesting to develop efficient techniques to detect and identify the types of disorders.

The presented method for detecting disturbances in the voltage waveforms using angular parameterization of orthonormal wavelet filter banks with regular functions shows a good performance. For all the analyzed cases, the detection was accurate, showing the beginning and end of the disorder, of cases in which they are present in the signal.

The scalogram signal decomposed by the same wavelet with three vanishing moments reveals the nature of the phenomenon that occurs in the signal, since visually the detail coefficients at different parts of the signal may look the same when it does not identify high frequency information.

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DOI: [10.19080/RAEJ.2018.03.555605](https://doi.org/10.19080/RAEJ.2018.03.555605)

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